

Welding Process Simulation and Fatigue Assessment of Railhead Repairs



Svetskommissionens forskningsseminarium

Stockholm, 2025-10-16

Björn Andersson, PhD

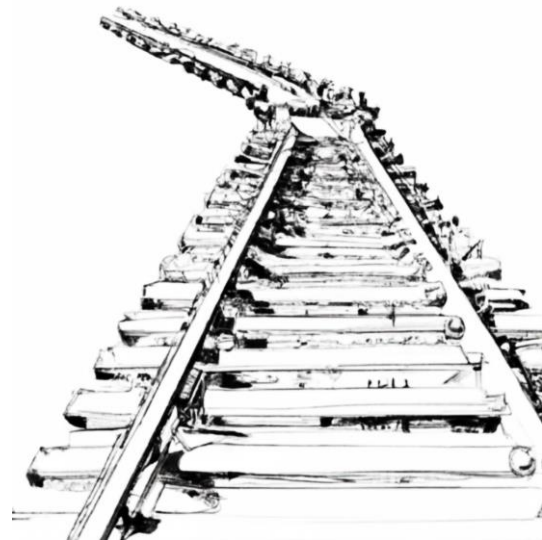
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Division of Material and Computational Mechanics

Department of Industrial and Materials Science

CHARMEC (Chalmers Railway Mechanics)

Chalmers University of Technology



Department of Industrial and Materials Science

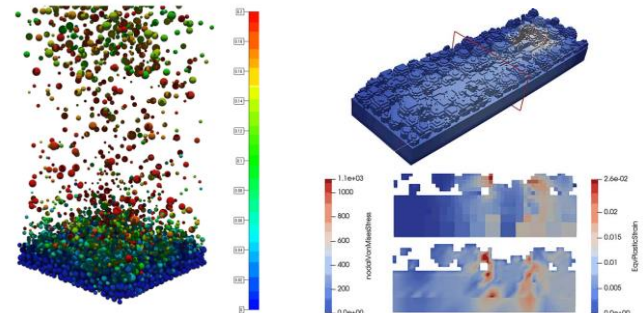
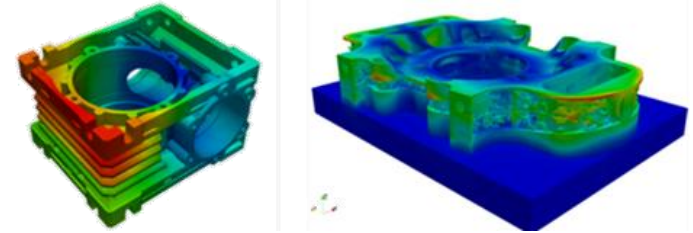
- Division of Material and Computational Mechanics
- Division of Product Development
- Division of Engineering Materials
- Division of Materials and Manufacturing
(Centre for Additive Manufacture – Metal = CAM²)

Department of Architecture and Civil Engineering

- Division of Structural Engineering

Department of Physics

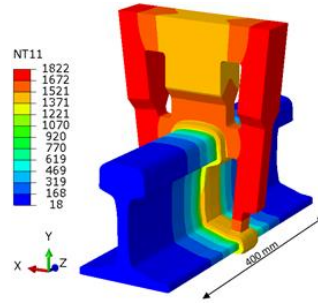
- Division of Microstructure Physics



Rail welding

CHARMEC (Chalmers Railway Mechanics)

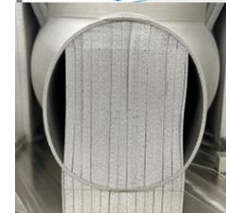
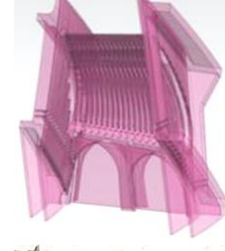
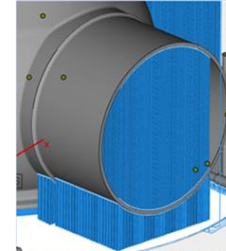
- Flash butt welding
- Thermite welding
- Orbital friction welding
- Repair welding (arc welding)

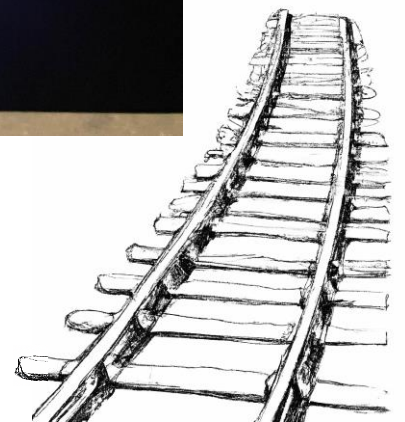


Powder Bed Fusion – Laser Beam (PBF-LB)

in collaboration with RISE

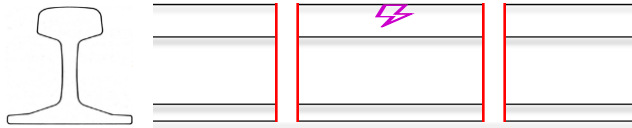
- High fidelity mesoscale submodel generating local inherent strains
- Macro scale (part model), distributed inherent strain





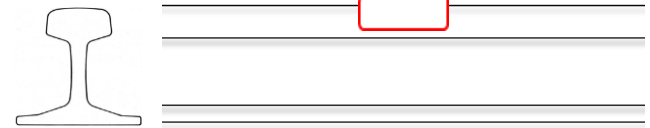
[1] <https://mp.nl/en/solution/sound-measurements-board-train-detecting-rail-defects>, [2] <https://www.raildamage.com/>

Rail section repair - Thermite welding



- Remove entire damaged rail section
- Large heat input
- Slower cooling, pearlite formation, tensile stresses in web

Rail head repair – MIG/MMA welding

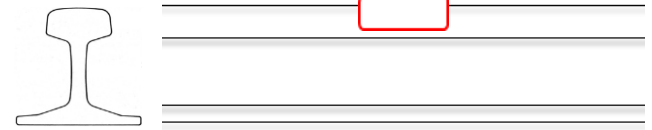


- Remove only railhead damage (or switches)
- Small, local heat input, several weld passes
- Rapid cooling, risk for martensite formation
- Complex microstructure evolution
- Effects of phases and phase transformations

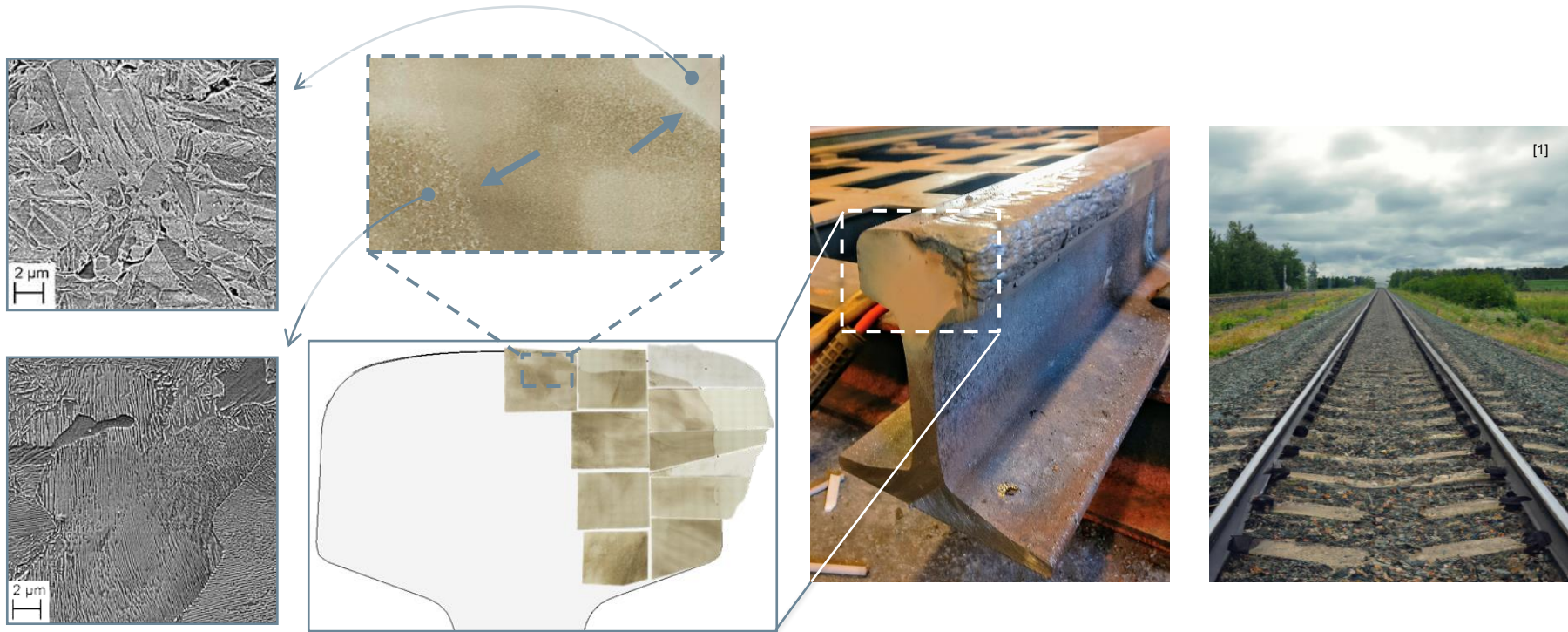
**Research goal:
Improve using mechanical
performance numerical simulations**

Rail Material R260
Fully Pearlitic (high carbon ~0.75%)
20-60% of all rail defects in weld regions

Rail head repair – MIG/MMA welding

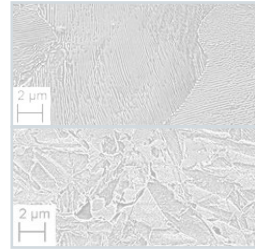
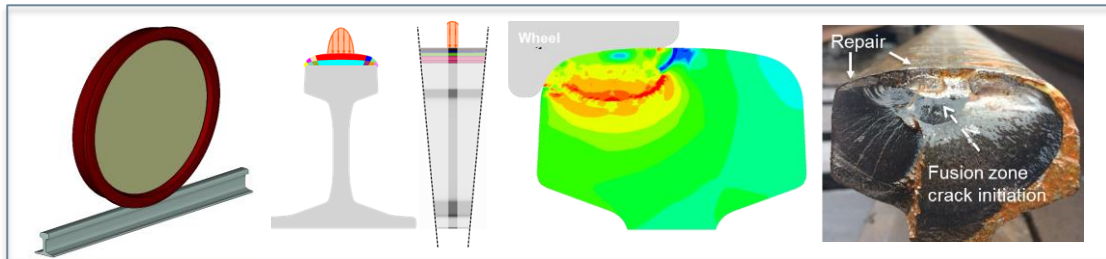
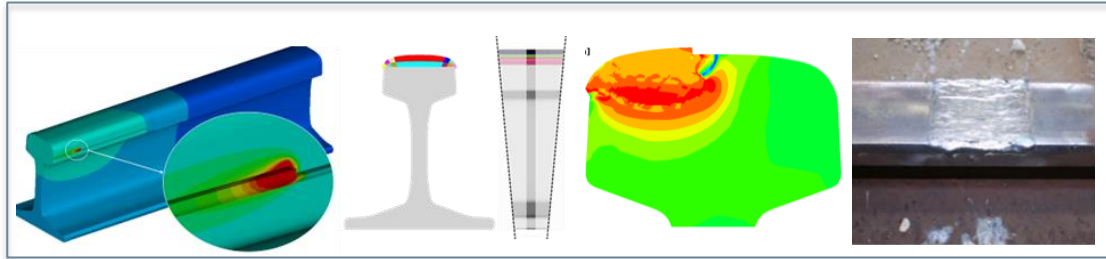
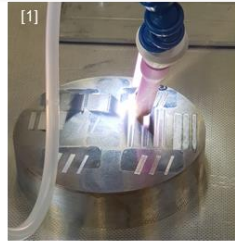
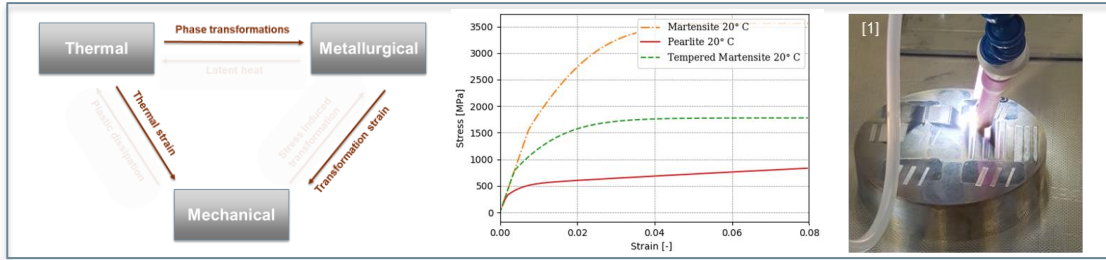


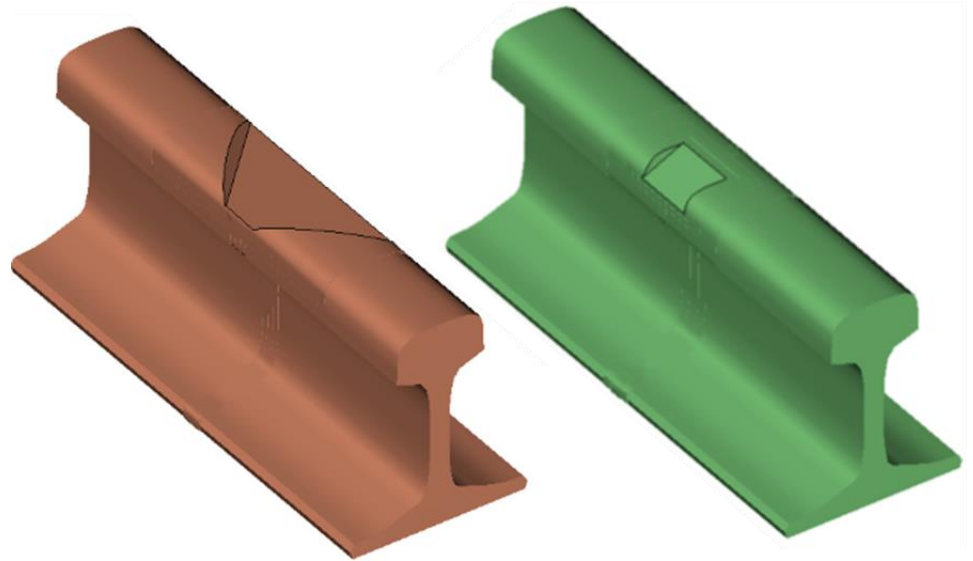
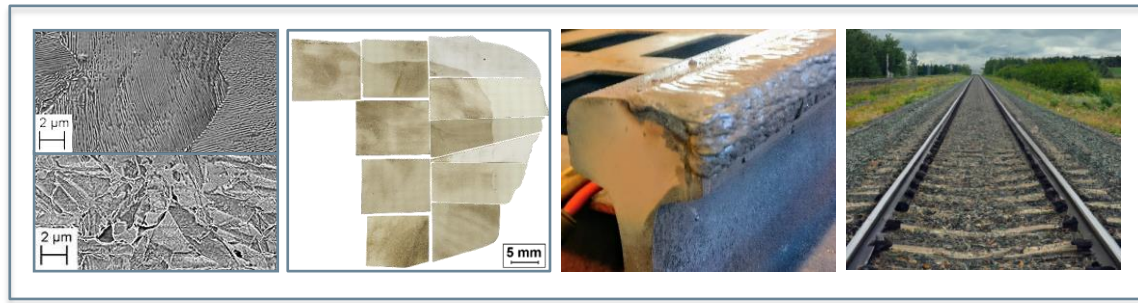
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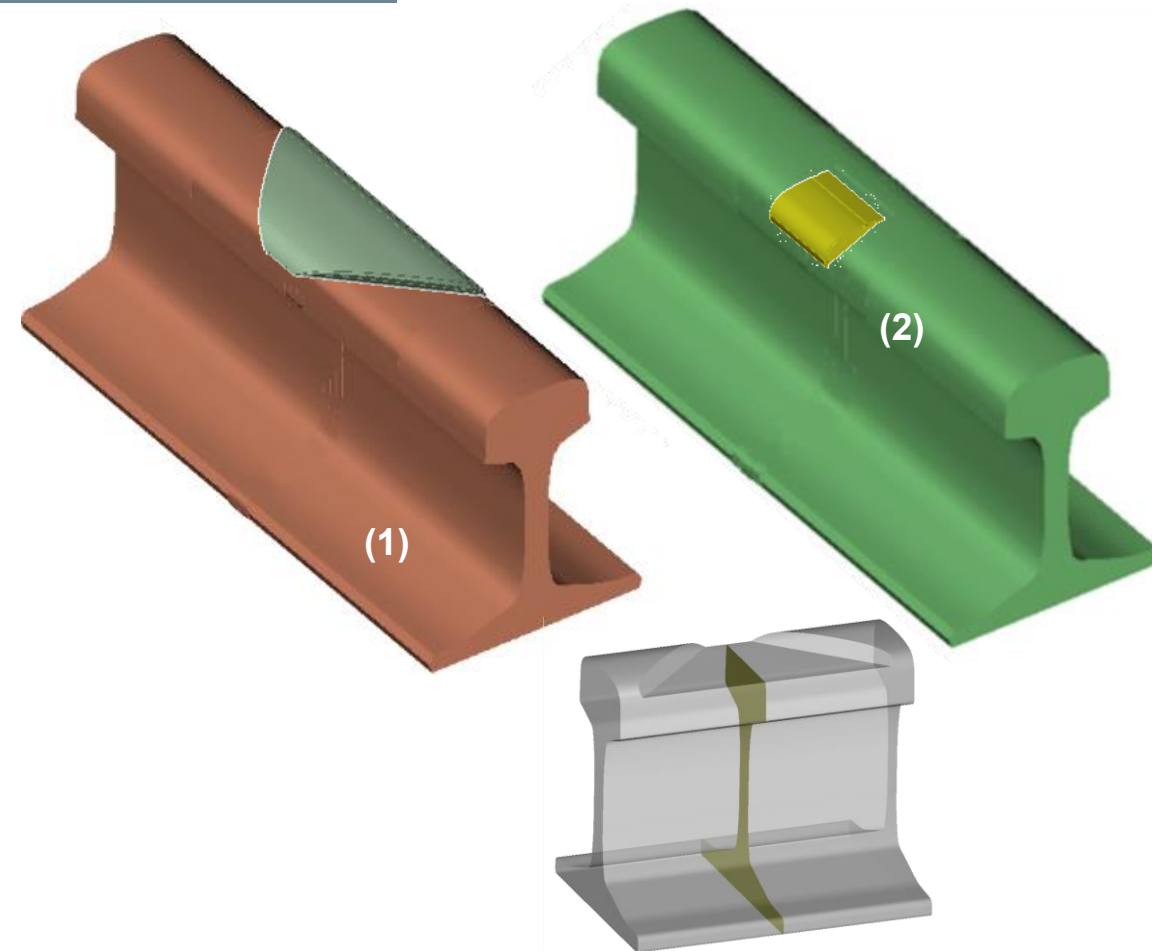




Rail repair welding simulation methodology







Railhead repair welding procedure::

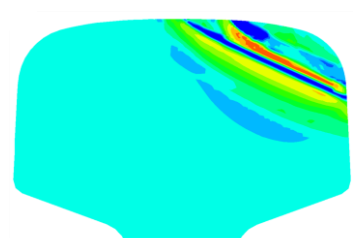
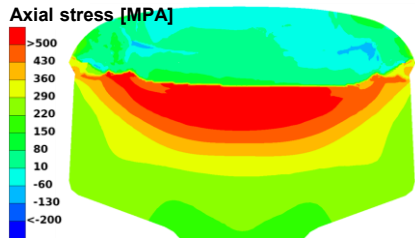
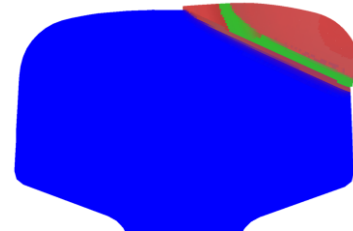
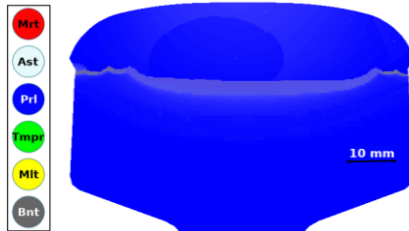
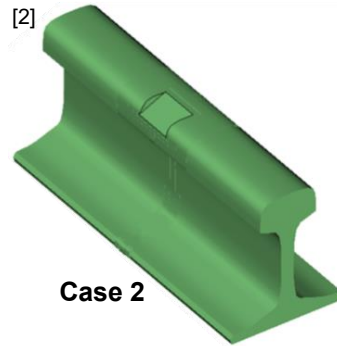
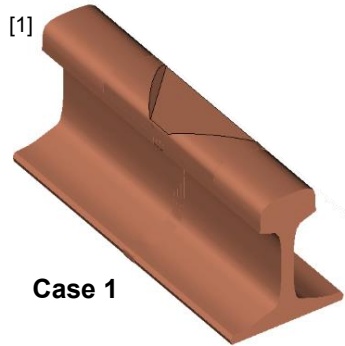
- 350°C preheat (and reheat)
- Manual Metal Arc Welding
- Filler material: Weartrode 30

Case 1

- Following Swedish regulations
- 10 mm deep cut-out
- 45° chamfered cutouts
- Longitudinal support ridge weld passes
- Zig-zag weld passes between ridges

Case 2

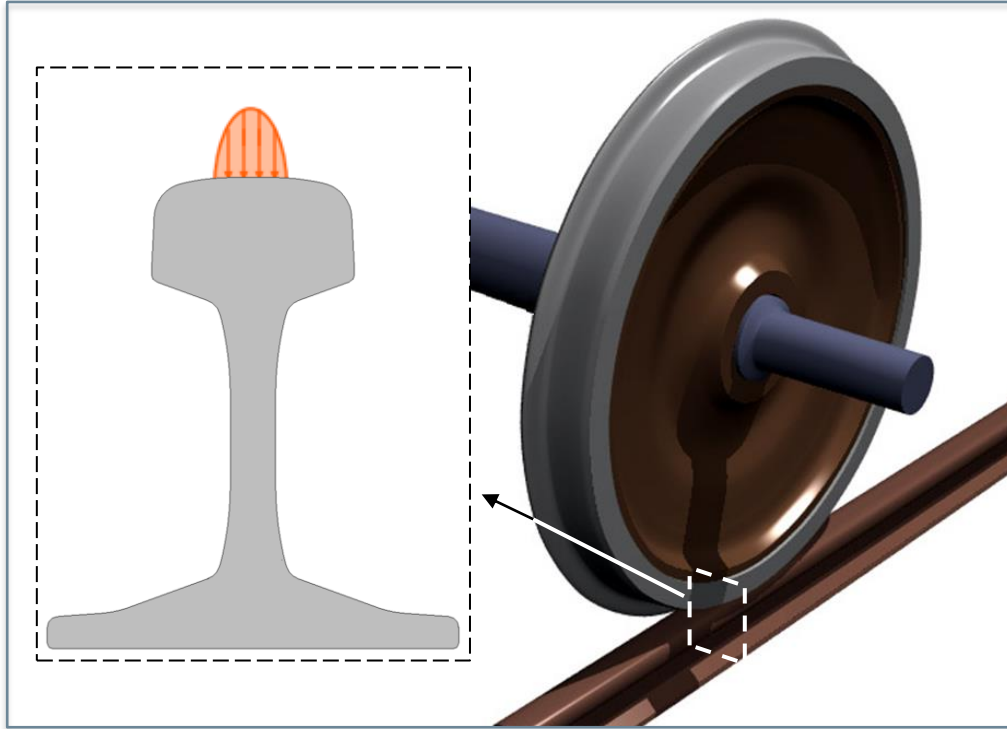
- Typical faulty repair procedure
- Rail corner cut-out
- 10 mm deep cut-out (at max point)
- 50 mm long cut-out
- 25° slope

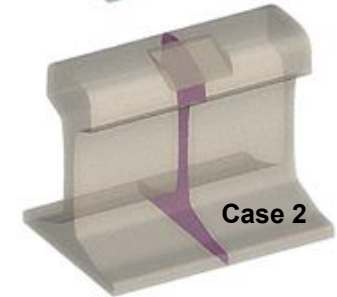
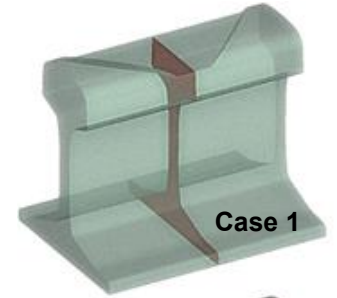
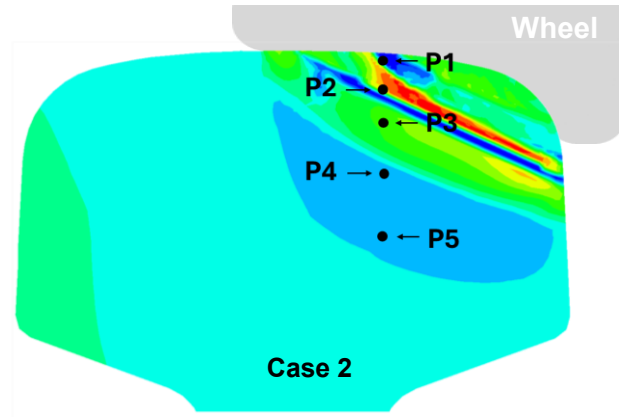
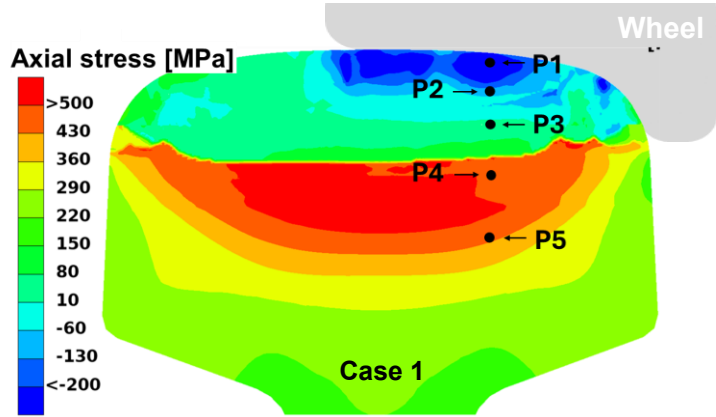


- Geometry significantly effects:
 - Heat input
 - Residual stress state
 - Material phases
 - Mechanical performance
- Smaller repairs:
 - Less heat input
 - Rapid cooling
 - Unfavorable microstructure
 - Impaired performance
- Case 1 (Trapezoid shape):
 - Large heat input with smooth ramp up and ramp down
 - Improved performance

[1] Andersson, *et al.* Simulation-based assessment of railhead repair welding process parameters. *Weld World* 69, 177–197 (2025)

[2] Andersson & Josefson, Simulation-based failure analysis of faulty and regulatory railhead repair welding procedures, *Engineering Failure Analysis*, Volume 182 (2025)





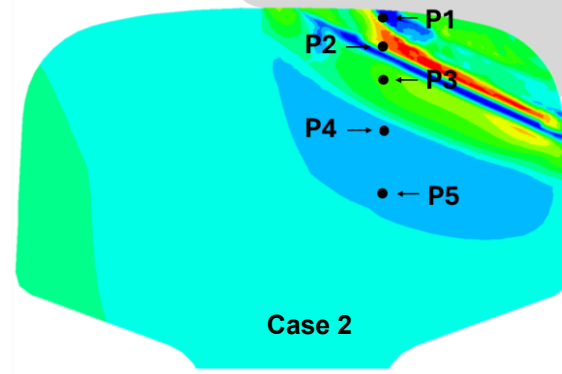
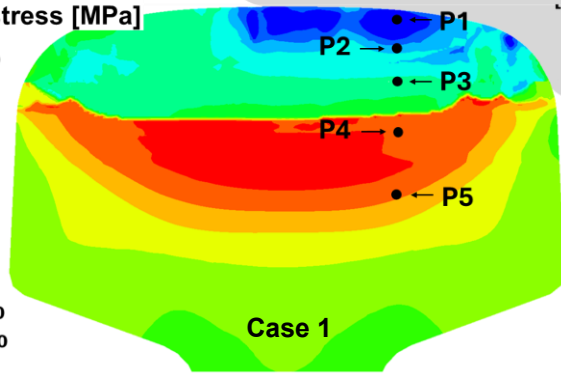
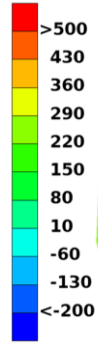
Post repair weld operational condition fatigue evaluation

- Load 20 trains on Swedish western main line
- Load repeated 4 times: **2000 over-rollings**
- Residual stress weld + over-rollings
- Fatigue evaluation (crack initiation) using Dang Van method

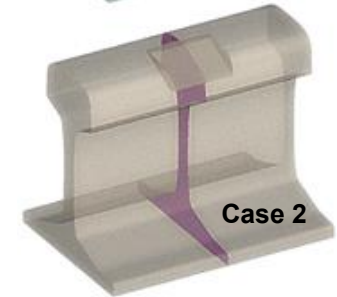
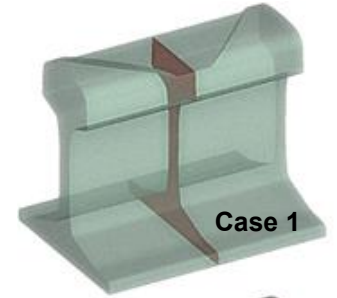
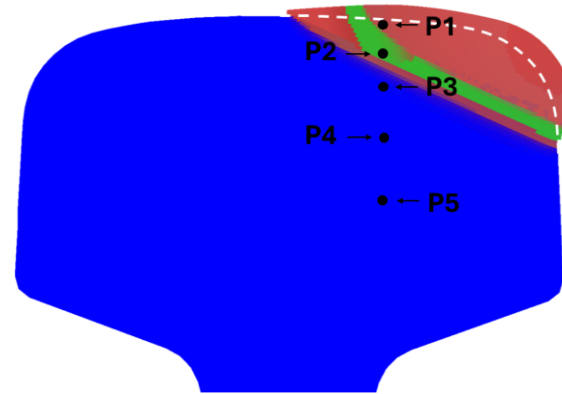
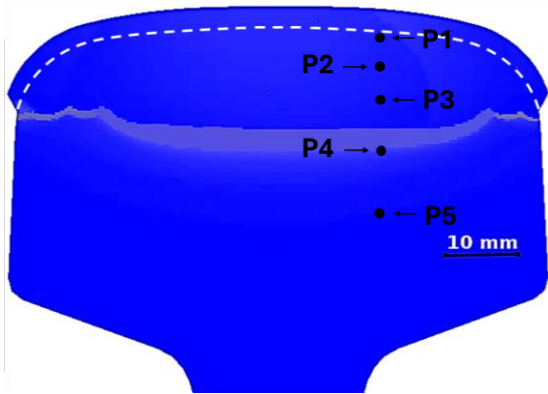
$$\sigma_{eq,DV}(t) = \tau_{Tr,a}(t) + \langle c_{DV}\sigma_h(t) \rangle < \tau_{e,i}$$

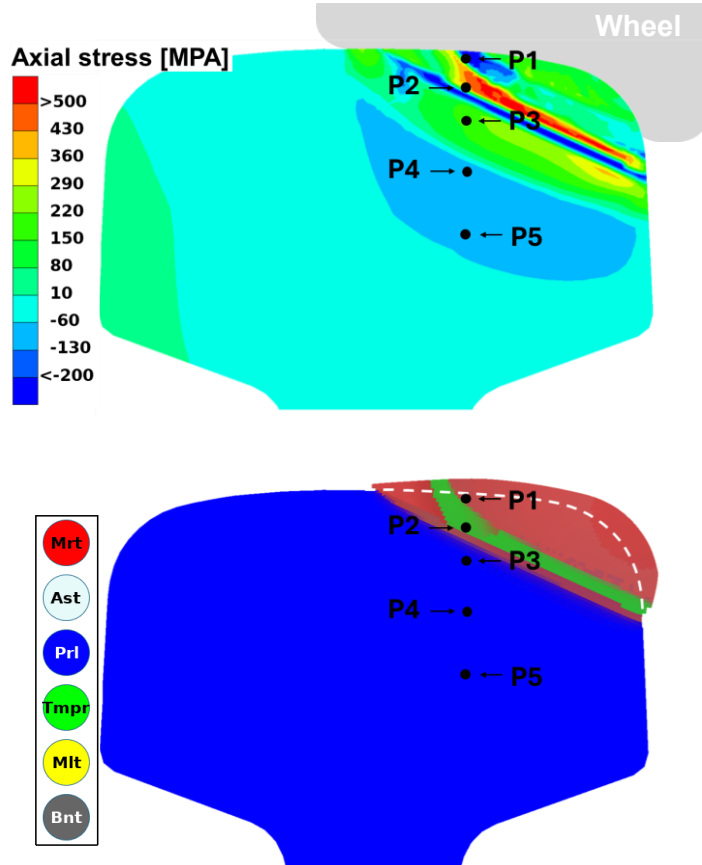


Axial stress [MPa]



- Mrt
- Ast
- Pri
- Tmpr
- Mit
- Bnt





Dang Van fatigue stress

$$\sigma_{DV}(t) = \tau_{Tr,a}(t) + \langle c_{DV,i} \sigma_h(t) \rangle > \tau_{e,i}$$

Shear stress fatigue limit and hydrostatic stress parameter

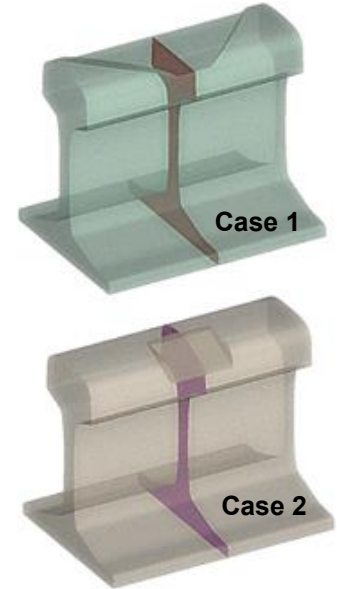
$$\tau_{e,i} = \frac{H_{V,i}}{H_{V,p}} \tau_{e,p}$$

$$c_{DV,i} = 3 \left(\frac{\tau_{e,i}}{\sigma_{ew,i}} - \frac{1}{2} \right)$$

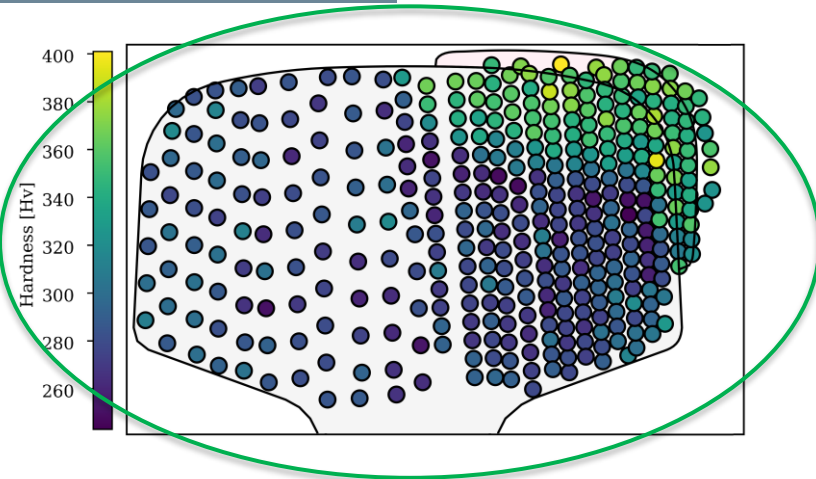
Alternating bending shear stress (Murakami [2])

$$\sigma_{ew,i} = \frac{1.56(H_{V,i} + 120)}{(\sqrt{area})^{1/6}}$$

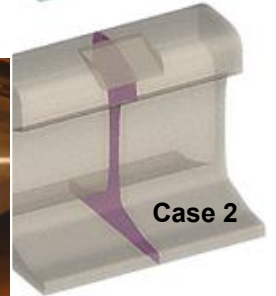
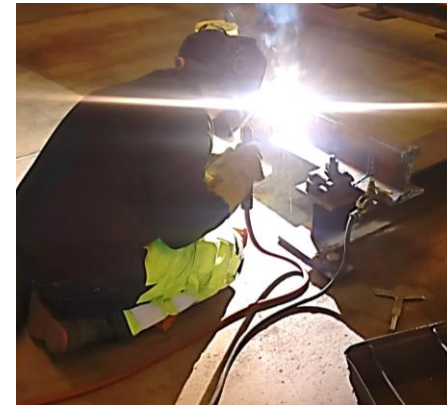
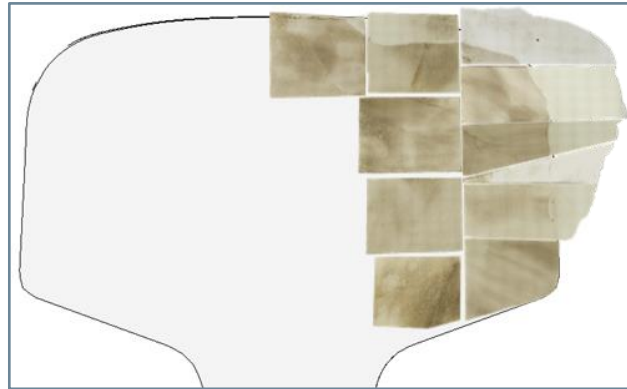
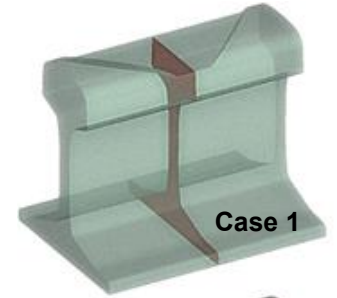
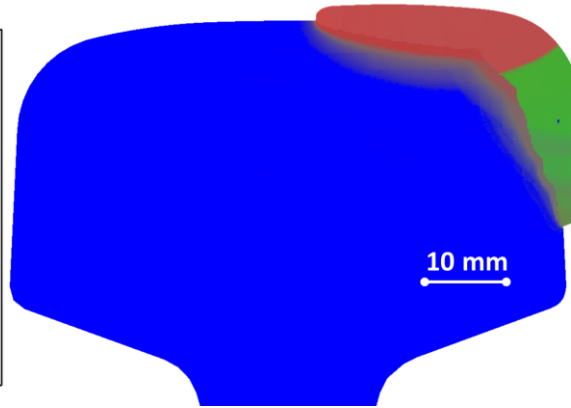
\sqrt{area} inherent subsurface material defect [3]



[1] Andersson & Josefson, Simulation-based failure analysis of faulty and regulatory railhead repair welding procedures, Engineering Failure Analysis, Volume 182 (2025)
 [2] Y. Murakami, M. Endo, Effects of defects, inclusions and inhomogeneities on fatigue strength Int. J. Fatigue, 16 (3) (1994), pp. 163-182
 [3] D. Franklin, A. Lundstjälk, LIVAR – Livslängsoptimering av räler: Tech. Rep., Swerim, Stockholm, Sweden (2021)

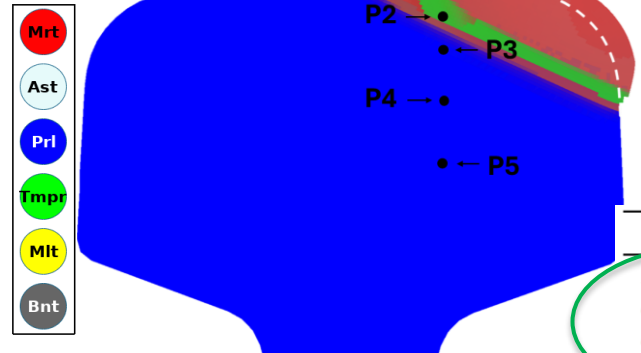
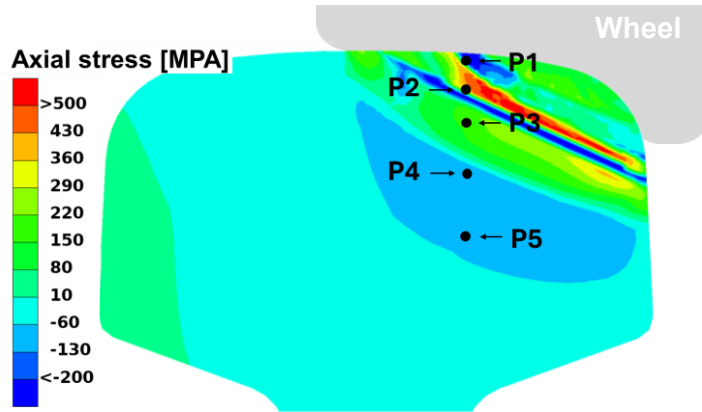


- Mrt
- Ast
- Pri
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Repair welding and over-rolling simulation



Dang Van fatigue stress

$$\sigma_{DV}(t) = \tau_{Tr,a}(t) + \langle c_{DV,i} \sigma_h(t) \rangle > \tau_{e,i}$$

Shear stress fatigue limit and hydrostatic stress parameter

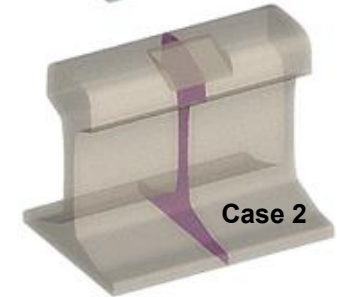
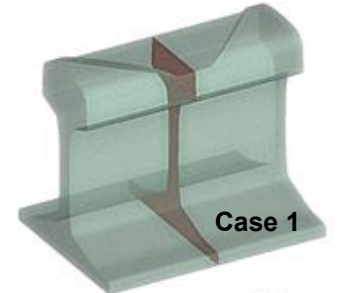
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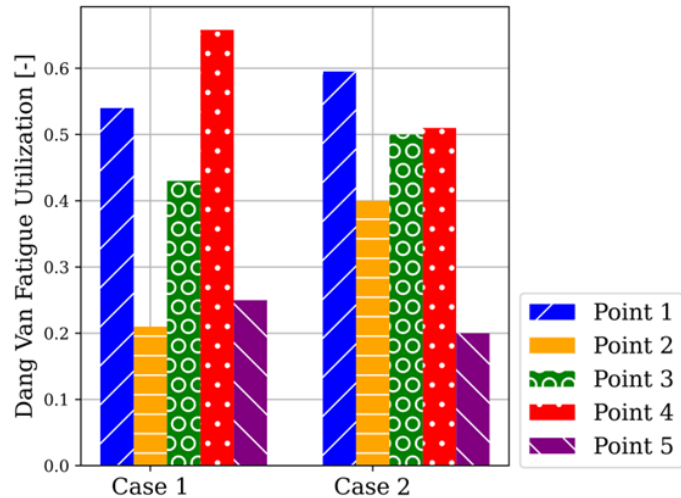
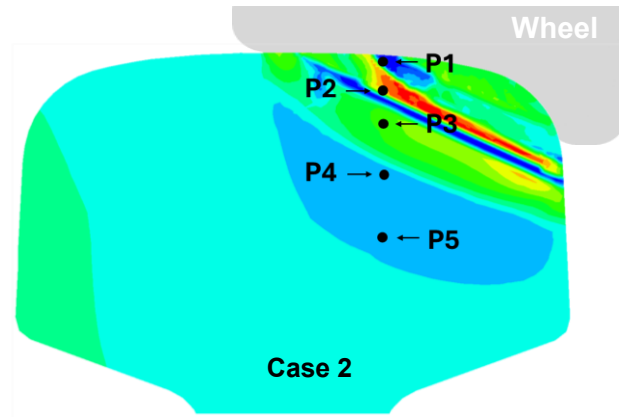
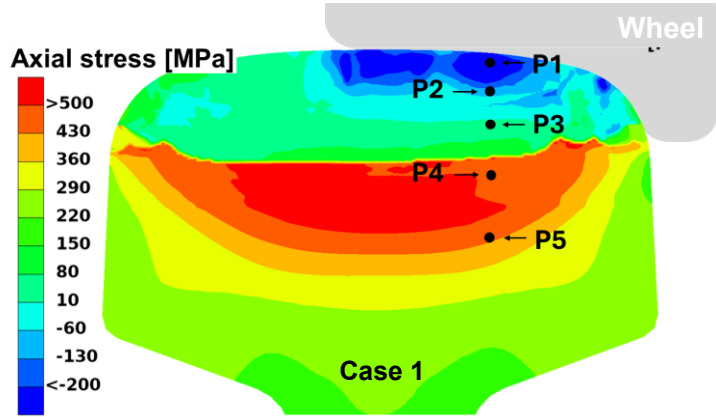
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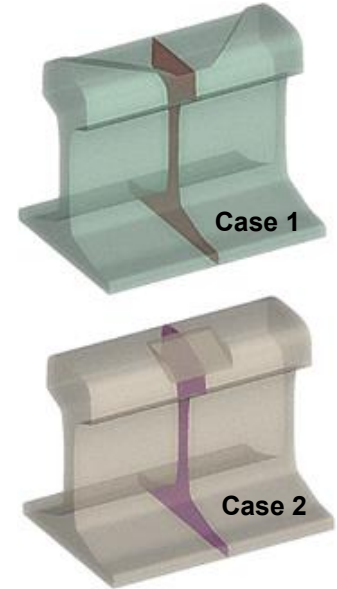
H_V [kgf/mm ²]	275	520	420	340
c_{DV} [-]	0.33	0.64	0.55	0.44
σ_{ew} [MPa]	275	446	376	320
τ_e [MPa]	168	318	257	208

	Pearlite	Martensite	Bainite	Tempered
H_V [kgf/mm ²]	275	520	420	340
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- Fatigue evaluation (crack initiation) using Dang Van method
- $\sigma_{eq,DV}(t) = \tau_{Tr,a}(t) + \langle c_{DV}\sigma_h(t) \rangle < \tau_{e,i}$
- Critical point at fusion zone
- Better mechanical performance for Case 1





Simulation-based Failure Analysis of Faulty and Regulatory Railhead Repair Welding Procedures

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⁵Alpha Laser, Göteborg

⁶Infranord AB, Karlstad

